



## Effect of vacuum annealing on the structural and optical properties of sputtered $\text{Cu}_4\text{O}_3$ thin films

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### ABSTRACT

$\text{Cu}_4\text{O}_3$  thin films were deposited by the reactive magnetron sputtering process on glass and Si (100) wafers. In order to investigate the thermal stability of the  $\text{Cu}_4\text{O}_3$  phase, the films were subjected to vacuum annealing treatment for one hour at various temperatures ranging from 200°C to 500°C. The samples were characterized by using EDS, XRD, SEM and UV–VIS. The phase transformation of  $\text{Cu}_4\text{O}_3$  into  $\text{Cu}_2\text{O}$  was obtained from 300°C (critical temperature). Increasing annealing temperature leads to compact morphology and the grain shape changing from elongated towards spherical. Due to this annealing the film structure presents coexistence of a  $\text{Cu}_4\text{O}_3$  and  $\text{Cu}_2\text{O}$  mixture where O atoms are lost in the Cu–O system. The UV–VIS analysis reveals a gradual increase in the transmittances from 55 to 70% with the increasing annealing temperature, while the band gap shows a maximum value ( $E_g = 2$  eV) at 500°C corresponding to the  $\text{Cu}_2\text{O}$  phase.

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## Introduction

Paramelaconite ( $\text{Cu}_4\text{O}_3$ ) with exclusive oxygen saturation has received a large technological interest in various field applications like photovoltaic, catalysis, lithium storage batteries and solar cells [1–7].  $\text{Cu}_4\text{O}_3$  is a metastable phase that has copper atoms in two valence state:  $\text{Cu}^{\text{I}}$  and  $\text{Cu}^{\text{II}}$  [1]. Thus, few research studies have devoted to study the properties of  $\text{Cu}_4\text{O}_3$  thin films. Koenig et al. have determined its composition and crystal class as they named it melaconite [2]. Next, O'Keeffe and Bovin found that the  $\text{Cu}_4\text{O}_3$  composition should be presented by  $\text{Cu}(\text{I})_2\text{Cu}(\text{II})_2\text{O}_3$  [3,4]. Hsueh et al. have deposited  $\text{Cu}_4\text{O}_3$  nanowires by using magnetron sputtering to develop  $\text{Cu}_4\text{O}_3/\text{ZnO}$  photodiodes [5]. Recently, H.S. Kim et al. have elaborated devices based on  $\text{Cu}_4\text{O}_3$  for photodetector applications [8]. However, the use of  $\text{Cu}_4\text{O}_3$  thin films in various applications needs a good quality of materials, in terms of structural, optical and electrical properties. The enhanced properties of  $\text{Cu}_4\text{O}_3$  films can be achieved by changing the microstructure and chemical composition. This is typically controlled by the deposition parameters and the applied treatment. Knowing that  $\text{Cu}_4\text{O}_3$  is a metastable phase, heat treatment influences their structure properties. Therefore, vacuum and air annealing can transform  $\text{Cu}_4\text{O}_3$  into  $\text{Cu}_2\text{O}$  or  $\text{CuO}$ . Pierson et al. have

studied the thermal stability in air of the different copper oxide films at 300°C, 350°C and 400°C during 4 h. They found that the thermal conversion of  $\text{Cu}_2\text{O}$  and  $\text{Cu}_4\text{O}_3$  into  $\text{CuO}$  with an increase of the resistivity with a slight decrease of a stable  $\text{CuO}$  phase at the same temperature (350°C) [7]. D.S. Murali et al. have studied the effect of the thermal treatment on  $\text{Cu}_4\text{O}_3$  films by using the high-temperature Raman analysis. They found that the transition of  $\text{Cu}_4\text{O}_3$  to the  $\text{CuO}$  phase after annealing of the Cu–O films at 410°C and 450°C in ambient air and argon atmosphere, respectively [9]. Vacuum annealing of Cu–O films shows enhanced electrical and optical properties for  $\text{Cu}_2\text{O}$  thin films [10].

However, only limited reports on sputtered Cu–O films are available; these are either discussing the thermal stability of  $\text{Cu}_4\text{O}_3$  in vacuum annealing [10], or the influence of oxygen content on the optical and electrical properties without comprehensive information on the chemical and structural properties [9]. The major advantage of vacuum annealing is that it provides uniformity in the structure due to the atoms' rearrangement without oxygen insertion [11].

In this paper, we have deposited the  $\text{Cu}_4\text{O}_3$  thin films using DC magnetron sputtering. Then, the films were annealed under vacuum at different temperatures from 200°C to 500°C. The aim of this work is to study the  $\text{Cu}_4\text{O}_3$  thermal stability and to investigate the

correlation between heat treatment and structural properties. The impact of vacuum annealing on the optical behaviour, especially the band gap of each phase as well as that of the mixture ( $\text{Cu}_4\text{O}_3 + \text{Cu}_2\text{O}$ ), was also studied.

## Experimental and details

### Film deposition

$\text{Cu}_4\text{O}_3$  films were deposited by a DC magnetron sputtering process in a reactive mode (Alcatel SCM600) at a total working pressure ( $\text{Ar} + \text{O}_2$ ) of 0.5 Pa and a Cu discharge current of 1A. The Cu target (99.9% purity, 200 mm diameter) was fixed on a magnetron-effect cathode. The substrate holder was situated in front of the target at 140 mm distance and with an angle of  $90^\circ$  from the normal, to obtain films uniform thickness. The details of the deposition conditions used in this work have been reported in the literature [11]. Before the deposition procedure, the process chamber was evacuated to a vacuum of  $10^{-4}$  Pa.

The substrates ( $2.5 \times 2.5 \text{ cm}^2$ ) and Si(100) wafers ( $1 \times 1 \text{ cm}^2$ ) were cleaned in an ultrasonic bath of acetone and ethanol solution for 5 min for each one. Thereafter, the substrates and targets were cleaned by Ar ion etching for 5 min and surface oxide layers or impurities were removed. The cleaning step was performed with the following conditions: argon flow rate of 50 sccm, pressure of 0.4 Pa, voltage of 450 V, power of 230 W.

Cu–O films were deposited by adjusting the voltage (power) of Cu target at 500 V (250 W) and using a constant working pressure at 0.5 Pa during 40 min in  $\text{O}_2$  (25 sccm) plus Ar (50 sccm) gas mixture. The floating temperature was  $68^\circ\text{C}$  during the deposition process.

### Thermal treatment

$\text{Cu}_4\text{O}_3$  films were annealed under vacuum at various temperatures ( $200^\circ\text{C}$ ,  $250^\circ\text{C}$ ,  $300^\circ\text{C}$ ,  $350^\circ\text{C}$ ,  $400^\circ\text{C}$ ,  $450^\circ\text{C}$ ,  $500^\circ\text{C}$ ) in a tubular furnace. The thermal cycle consisted of a ramp of  $10^\circ\text{C min}^{-1}$ , followed by maintaining at the desired temperature for 1 h. Finally, the cooling takes place under vacuum at a rate of about  $-10^\circ\text{C min}^{-1}$ . A diffusion pump insured the pressure of  $10^{-7}$  Pa.

### Film characterization

Film composition was determined by the Bruker electron probe X-ray micro-analyzer. The  $\text{Cu}_4\text{O}_3$  crystalline structure was analysed by X-ray diffraction (XRD) using a D8 advanced with a  $\text{Cu}_{K\alpha}$  radiation source (40 kV, 40 mA,  $\lambda_{\text{Cu}} = 0.154 \text{ nm}$ ). The crystallite size ( $D$ ) was estimated from the full width at half-

maximum of the (002), (400) and (004) of  $\text{Cu}_4\text{O}_3$  phase and (111)  $\text{Cu}_2\text{O}$  orientations using the Scherrer's formula [12]:

$$D = \frac{0.94\lambda}{\beta \cos \theta} \quad (1)$$

where 0.94 is a shape factor,  $\lambda$  represents the X-ray wavelength of the radiation source used for the measurement ( $\lambda_{\text{Cu}} = 0.154 \text{ nm}$ ),  $\beta$  (rad) is the line full width at half-maximum and  $\theta$  is the Bragg's angle.

The lattice parameter ( $c$ ) for each orientation on the  $\text{Cu}_4\text{O}_3$  tetragonal phase was determined by the inter-reticular equation:

$$d_{hkl} = \frac{ac}{\sqrt{c^2(h^2 + k^2) + a^2l^2}} \quad (2)$$

In addition, the  $\text{Cu}_2\text{O}$  cubic phase was evaluated by

$$d_{hkl} = \frac{a}{\sqrt{h^2 + k^2 + l^2}} \quad (3)$$

The microstrains of  $\text{Cu}_4\text{O}_3$  or  $\text{Cu}_2\text{O}$  phases were calculated using the following equation:

$$\varepsilon = \frac{\Delta d}{d_{\text{bulk}}} \quad (4)$$

where  $\varepsilon$  is the microstrain in the direction of the  $c$  axis, i.e. perpendicular to the substrate surface  $\Delta c = c_{\text{film}} - c_{\text{bulk}}$ ,  $d_{\text{film}}$  and  $d_{\text{bulk}}$  of  $\text{Cu}_4\text{O}_3$  or  $\text{Cu}_2\text{O}$  phases.

The cross-section and the surface morphologies were observed by using a field emission scanning electron microscope (FE-SEM-Hitachi-SU8030).

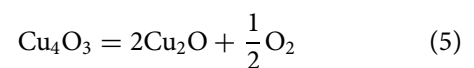
The average roughness  $R_a$  was measured with an atomic force microscope (AFM 100, APE research), which was employed under contact mode with the scan range of  $3 \times 3 \mu\text{m}$ .

The transmittance of the annealed  $\text{Cu}_4\text{O}_3$  films was measured by using a Perkin Elmer UV–VIS Lambda 19 spectrophotometer in the 190–1100 nm spectral range.

## Results and discussion

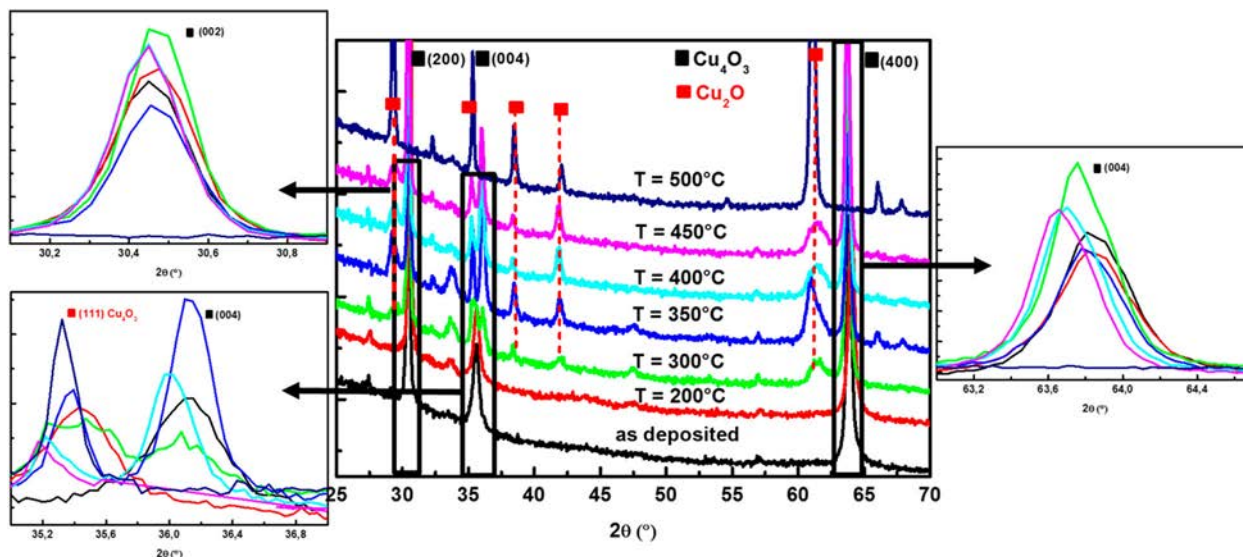
### Structure and chemical composition

The  $\text{Cu}_4\text{O}_3$  and  $\text{Cu}_2\text{O}$  phases differ from each other in the stoichiometric ratio. The reduction of  $\text{Cu}_4\text{O}_3$  to  $\text{Cu}_2\text{O}$  is governed by the endothermic reaction [13]:



Thus, energy from a vacuum annealing is needed to convert the  $\text{Cu}_4\text{O}_3$  into  $\text{Cu}_2\text{O}$ .

The O/Cu atomic ratio of the as-deposited film was found to be 3/4. However, the increase of vacuum annealing temperature leads to a drop in the O/Cu atomic ratio down to 1/2 at  $500^\circ\text{C}$ . According to Sun H. et al., the increase of annealing temperature caused



**Figure 1.** XRD evolution of copper oxides films at different vacuum annealing temperatures.

the movement of oxygen atoms out of the Cu crystal lattices and the formation of copper oxide compounds with low oxygen content [14]. This is due to the relative reduction of oxygen during vacuum annealing treatment.

Figure 1 presents the XRD patterns of  $\text{Cu}_4\text{O}_3$  films (960 nm thick) before and after vacuum annealing treatments. Before vacuum annealing, the films revealed peaks at  $30.96^\circ$ ,  $36.11^\circ$  and  $61.26^\circ$ , corresponding to (200), (004) and (400) crystallographic orientation of the tetragonal  $\text{Cu}_4\text{O}_3$  phase (JCPDS Card # 49-1830). Below  $300^\circ\text{C}$ , the same peaks were observed, this indicates that no phase transformation occurred. J.F. Pierson et al. found the same structure by using the RF magnetron sputtered  $\text{Cu}_4\text{O}_3$  films [15]. Between  $350^\circ\text{C}$  and  $450^\circ\text{C}$ , new weak peaks (110), (111) and (220) have appeared at  $29.55^\circ$ ,  $36.42^\circ$  and  $61.34^\circ$ , corresponding to the cubic  $\text{Cu}_2\text{O}$  phase (JCPDS Card # 5-0667). In our case, XRD analysis confirms the total transformation of  $\text{Cu}_4\text{O}_3$  to  $\text{Cu}_2\text{O}$  at  $500^\circ\text{C}$ . The disappearance of the  $\text{Cu}_4\text{O}_3$  phase is observed and the  $\text{Cu}_2\text{O}$  phase becomes dominated by the appearance of the predominant (111) peak at  $500^\circ\text{C}$  that confirms the total transformation of  $\text{Cu}_4\text{O}_3$  to  $\text{Cu}_2\text{O}$ . Similar behaviour was observed by J. Sohn et al., which found that the transformation of the monoclinic  $\text{CuO}$  into cubic  $\text{Cu}_2\text{O}$  is accelerated at higher temperatures (at  $500^\circ\text{C}$ ) by the reducing

process [16–18]. Blobaum et al. found that Gibbs free energy of  $\text{Cu}_4\text{O}_3$  formation is  $-40 \text{ kJ} \cdot (\text{mol atom})^{-1}$ , which is less than that of  $\text{Cu}_2\text{O}$  ( $-39.22 \text{ kJ} \cdot (\text{mol atom})^{-1}$ ), indicating the thermodynamic instability of bulk  $\text{Cu}_4\text{O}_3$  at elevated temperatures [19]. Therefore,  $300^\circ\text{C}$  is the critical temperature of phase transformation of  $\text{Cu}_4\text{O}_3$  under vacuum annealing.

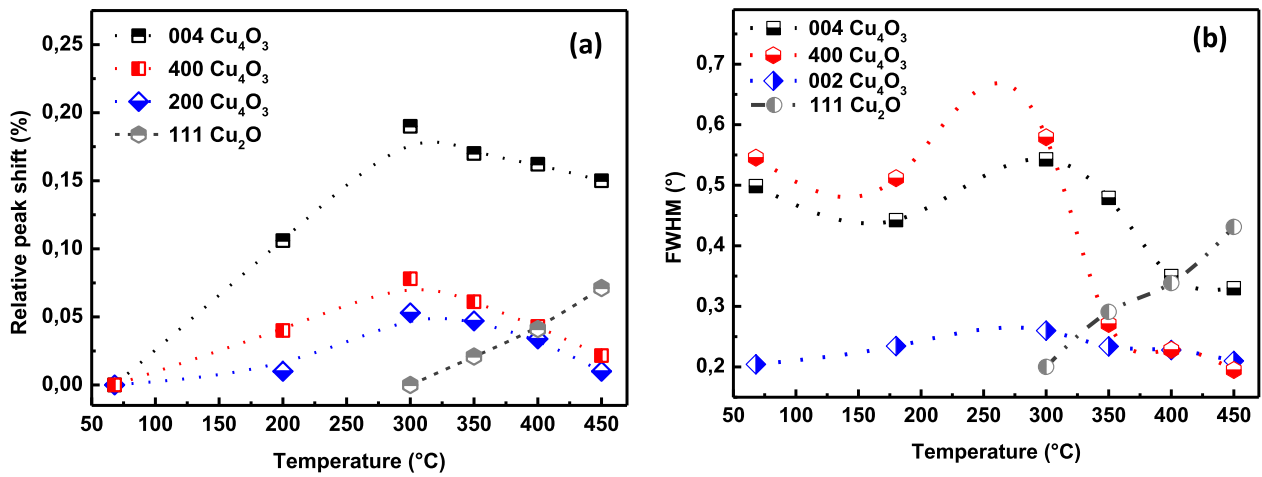
Residual microstrains ( $\epsilon$ ) of  $\text{Cu}_4\text{O}_3$  films as a function of annealing temperature are presented in Table 1. All films are in compressive stress state. The increasing temperature leads to the gradual decrease in the microstrains from  $-0.365$  (before annealing) to  $-0.0812\%$  (at  $500^\circ\text{C}$ ). This may be attributed to the relaxation of the stresses and the decrease in the  $\text{Cu}_4\text{O}_3$  lattice parameter that is the result of the thermal treatment [11].

Figure 2 shows the full width at half-maximum (FWHM) and the peaks shift as a function of annealing temperature for Cu–O films. These results were obtained for both  $\text{Cu}_4\text{O}_3$  and  $\text{Cu}_2\text{O}$  phases. Increasing the annealing temperature obviously leads to a significant increase in the increase of FWHM and peaks shift.

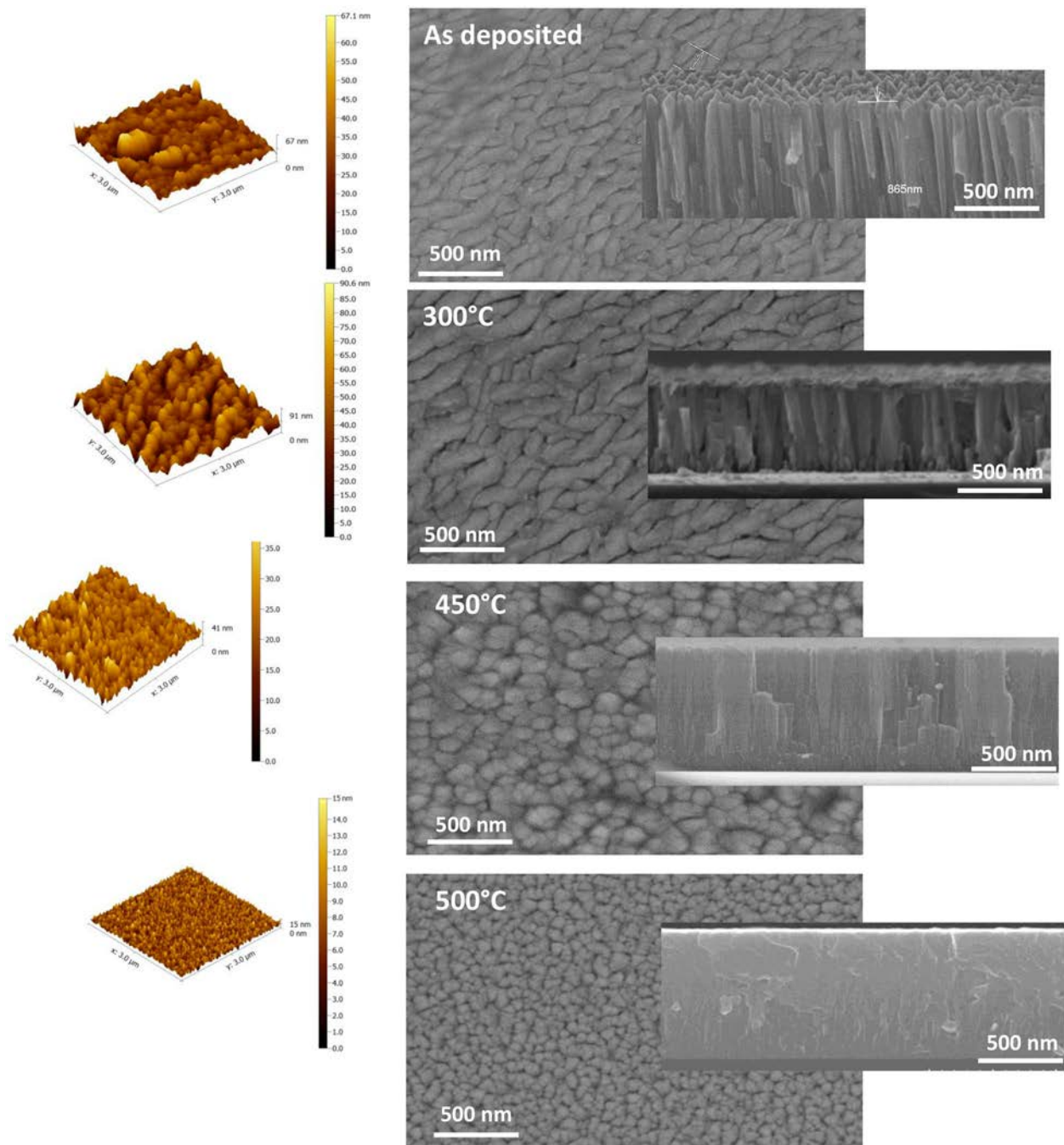
These changes in  $\text{Cu}_4\text{O}_3$  FWHM and peaks positions suggest that the relaxation of the  $\text{Cu}_4\text{O}_3$  lattice follows progressively as the oxygen content in the films decreases. Loss of oxygen leads to a progressive conversion of  $\text{Cu}_4\text{O}_3$  phase to  $\text{Cu}_2\text{O}$ , resulting in a severe decrease in intensity that accompanied with an

**Table 1.** Evolution of  $d_{hkl}$  and microstrains of  $\text{Cu}_4\text{O}_3$  and  $\text{Cu}_2\text{O}$  phases as a function of annealing temperatures.

T(°C)	( $\text{Cu}_4\text{O}_3$ ) $d_{200}$	( $\text{Cu}_4\text{O}_3$ ) $d_{004}$	( $\text{Cu}_4\text{O}_3$ ) $d_{400}$	( $\text{Cu}_2\text{O}$ ) $d_{111}$	E (%)
As-deposited	2.933	2.848	1.5500	/	0.242
200	2.922	2.845	1.5510	/	0.181
300	2.919	2.844	1.5498	2.456	-0.365
350	2.914	2.833	1.5482	2.459	-0.243
400	2.915	2.835	1.5486	2.460	-0.203
450	2.916	2.838	1.5489	2.461	-0.162
500	/	/	/	/	-0.081



**Figure 2.** (a) Relative shift, (b) FWHM of (200), (004) and (400)  $\text{Cu}_4\text{O}_3$  and (111)  $\text{Cu}_2\text{O}$  peaks at different vacuum annealing temperatures.



**Figure 3.** Top-view and cross-section SEM images and AFM topography of  $\text{Cu}_4\text{O}_3$  as-deposited heated thin films at different vacuum annealing temperatures.

**Table 2.** Evolution of crystallite size as a function of annealing temperatures.

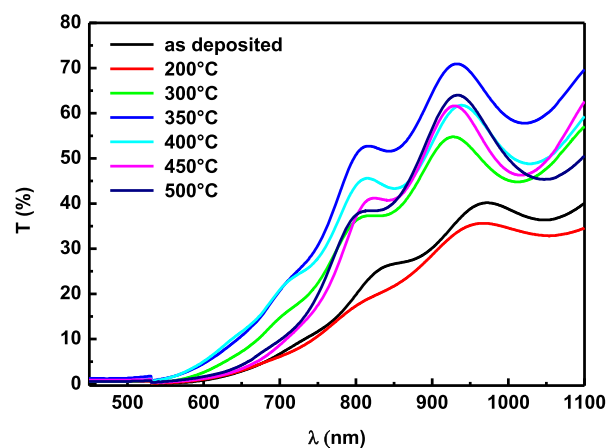
Cryst size (nm)/T(°C)	(200)Cu <sub>4</sub> O <sub>3</sub>	(004)Cu <sub>4</sub> O <sub>3</sub>	(400)Cu <sub>4</sub> O <sub>3</sub>	(111)Cu <sub>2</sub> O
As-deposited	30.82	17.96	18.59	/
200	34.76	19.02	19.92	/
300	32.21	35.65	23.34	33.71
350	36.57	38.14	21.81	29.34
400	37.83	36.71	20.34	28.33
450	36.74	34.65	20.09	27.76
500	/	/	/	15.28

increase in FWHM of the (111) Cu<sub>2</sub>O. This is due to the poor crystallization of Cu<sub>4</sub>O<sub>3</sub> and the relatively low oxygen content in the film. Film structure evolution is related to the compressive microstrains introduced in the film, during annealing treatment, via the complex nature of reaction between copper and oxygen atoms [11,17].

Below 300°C, the XRD peaks of the tetragonal Cu<sub>4</sub>O<sub>3</sub> phase slightly shift to higher diffraction angles, suggesting a small lattice distortion (Figure 2(a)). From 300°C to 500°C, XRD peaks shift to lower diffraction angles that indicate the increase of lattice parameter. This is explained by increasing microstructural strain or crystallite size effects in the film [17].

Figure 3 shows the FESEM and the AFM images of Cu<sub>4</sub>O<sub>3</sub> films deposited on silicon substrates. It is obvious that the morphology of the deposited film depends on annealing temperature. Before vacuum annealing, the film surface presents homogenous elongated grains with a mean crystallite size of 20 nm (Table 2). At 300°C, the film shows the same grain shape as before vacuum annealing, with the enlargement of grain size, indicating an improvement in crystallinity.

Before annealing, the Cu<sub>4</sub>O<sub>3</sub> film exhibits a dense columnar structure with elongated grains, which is a result of high working pressures (0.5 Pa) (Figure 3). The crystallite size and the roughness are 19 nm. Moreover, the AFM topography of the Cu–O films has

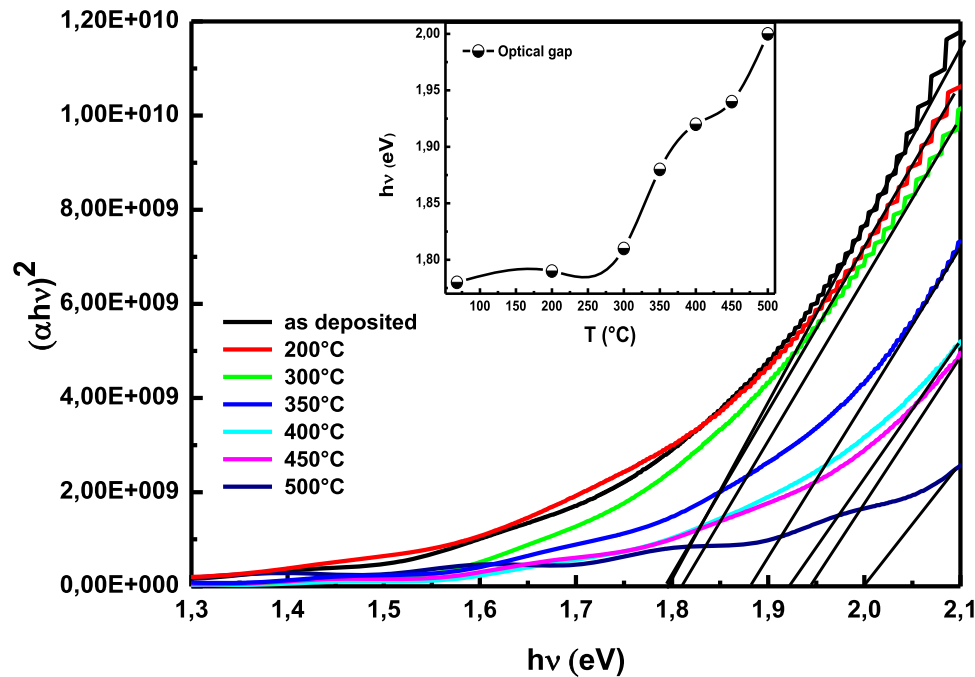
**Figure 4.** Optical transmittance spectra of the Cu–O thin films at different vacuum annealing temperatures.

coarse irregular tops surrounded by large voids with large grains and high roughness (67.1 nm). Similar morphology evolution has been reported in the literature [11,18]. At 300°C, the film presents the same grain morphology as before vacuum annealing, with a grain size enlargement. The mean crystallite size and the film roughness of the Cu<sub>4</sub>O<sub>3</sub> films are clearly increased (31 and 90.6 nm), respectively. Above 300°C, temperature increasing leads to the changing in the structure. At 450°C, the films exhibit more compact morphology than that of as-deposited films. The grain becomes spherical like form, which corresponds to the Cu<sub>2</sub>O phase [9]. These grains become finer at 500°C with a crystallite size of 25 nm. Thus, the grains (Ra = 15 nm) become smooth and homogeneous tops with small voids that might be due to recrystallization of the films [15,16].

### Optical property

Figure 4 shows the UV–VIS spectra of Cu<sub>4</sub>O<sub>3</sub> films, before and after annealing treatment, at different temperatures. As-deposited and 200°C annealed paramelacnite films show an average transmittance of 38%. An average transmittance of 55% is observed in the film annealed at 300°C. However, between 350°C and 450°C, the films that consist of a mixture of Cu<sub>4</sub>O<sub>3</sub> + Cu<sub>2</sub>O phases show an average transmittance of 66%. At 500°C, the film that has been completely transformed to Cu<sub>2</sub>O, as confirmed by the XDR analysis, shows an improvement on the transmittance, reaching a maximum value of 70%. This enhancement in the transmittance is probably due to the crystallinity improvement [19]. In our case, vacuum annealing between 200°C and 500°C leads to the atom rearrangement of copper oxide structure. Temperature increase leads to larger grain size, as shown in Figure 3. The mechanism that can improve the transmittance properties is the reduction of grain-boundary scattering linked to the larger grain size of the film annealed at high temperature (Figure 5). Generally, the transmittance related to grain-boundary scattering in polycrystals is affected by the porosity, growth orientation and grain size. A low porosity means little scattering at pores. As the refractive indexes are dependent on grain orientations in some material, the refraction at the grain boundaries with different growth orientations will enhance, consequently the reduction of transmittance. Besides, at a given sample thickness, the small grain size will decrease the transmittance, as the light has to pass an increasing number of grain boundaries [20].

The value of the absorption coefficient for the strong absorption region of the thin film is determined by using the equation shown in reference [21]. The band gap energy of the annealing films was evaluated from the plot of  $(\alpha hv)^2$  as a function of the photon energy  $(hv)$  at the absorption edge of  $\alpha = 0$ . The values of



**Figure 5.** The plots of  $(\alpha hv)^2$  vs.  $h\nu$  of Cu–O films (960 nm) at different vacuum annealing temperatures.

the band gap ( $E_g$ ), as a function of the vacuum annealing temperature, are shown in Figure 5. Below 300°C, the  $\text{Cu}_4\text{O}_3$  films have an optical gap of 1.85 eV, which corresponds to the  $\text{Cu}_4\text{O}_3$  phase. W. Zheng et al. found that  $\text{Cu}_4\text{O}_3$  has an optical gap of 1.65 eV, which is lower than that of our result because of the improvement in the thin film crystallinity with annealing temperature [22]. From 350°C, the optical gap values take a value of 2 eV, which corresponds to the optical gap of the  $\text{Cu}_2\text{O}$  phase [23]. It can be seen that the band gap  $8(E_g)$  value ( $\sim 1.9$  eV) of the  $\text{Cu}_4\text{O}_3 + \text{Cu}_2\text{O}$  mixture phase is ranging between that of  $\text{Cu}_4\text{O}_3$  (1.8 eV) and  $\text{Cu}_2\text{O}$  (2 eV). Whatever the phase formed as a function of temperature, optical gap increase is observed.

## Conclusion

The effect of vacuum annealing treatment 500°C, on the morphological, structural and optical properties of  $\text{Cu}_4\text{O}_3$  thin films deposited at 0.5 Pa by DC reactive magnetron sputtering, was investigated. The study of the thermal stability of  $\text{Cu}_4\text{O}_3$  films allows us to highlight the following points.

The  $\text{Cu}_4\text{O}_3$  phase is stable below 300°C, with an increase in mean grain size and decrease in microstrains.  $\text{Cu}_4\text{O}_3 + \text{Cu}_2\text{O}$  phases mixture is found at a temperature ranging between 300°C and 450°C and a total transformation of  $\text{Cu}_4\text{O}_3$  to  $\text{Cu}_2\text{O}$  is obtained at 500°C.

As-deposited Cu–O films exhibit a dense columnar structure with elongated grains that become fine with spherical shape at 500°C, which corresponds to  $\text{Cu}_2\text{O}$ . The increasing temperature leads to an

improvement in the transmittance from 38% before annealing until 70% at 500°C.

A vacuum annealing was carried out to improve the optical property of Cu–O films; a high band gap value ( $E_g = 1.8$  eV) of the  $\text{Cu}_4\text{O}_3$  phase was obtained after vacuum annealing below 300°C.

## Disclosure statement

No potential conflict of interest was reported by the author(s).

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